

# Phase Equilibria in the Sodium Fluoride Enriched Region of the Reciprocal System $\text{Na}_6\text{F}_6\text{-Al}_2\text{F}_6\text{-Na}_6\text{O}_3\text{-Al}_2\text{O}_3$

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The location of univariant lines and invariant points in the sodium fluoride enriched region of the  $\text{Na}_6\text{F}_6\text{-Al}_2\text{F}_6\text{-Na}_6\text{O}_3\text{-Al}_2\text{O}_3$  reciprocal system were determined by refractive index and x-ray diffraction measurements of quenched samples. Two peritectic reaction points and one eutectic are defined.

The cryolite-sodium aluminate section is taken from the reciprocal diagram and plotted as conventional molar quantities. The section is shown to lack the qualities of a true system since  $\beta$ -alumina (the composition point of which is not located on the join) precipitates as primary phase.

THE RECIPROCAL system,  $\text{Na}_6\text{F}_6\text{-Al}_2\text{F}_6\text{-Na}_6\text{O}_3\text{-Al}_2\text{O}_3$  has been studied by Kostjukov (11). The planar square plot indicates that a univariant line separates the sodium fluoride and sodium aluminate phase fields in the NaF-rich region of the diagram. This line terminates at a peritectic invariant point where  $\beta$ -alumina also precipitates.

Recently published works on the NaF- $\text{Al}_2\text{O}_3$  system (8, 9) agree that this is the case, but the composition of the peritectic is at a much lower alumina content. Two other univariant lines originating at the cryolite-sodium fluoride and at the cryolite-alumina binary eutectics are shown by Kostjukov to join at an invariant eutectic point where the melt is triply saturated with respect to cryolite,  $\beta$ -alumina and sodium fluoride. The line joining the cryolite composition point at the 1:1  $\text{Na}_6\text{F}_6/\text{Al}_2\text{F}_6$  ratio and the  $\text{Al}_2\text{O}_3$  corner of the diagram is said to separate the  $\alpha$ - and  $\beta$ - $\text{Al}_2\text{O}_3$  phase fields. If that part of the cryolite-alumina join which cuts across the alumina phase field represents univariant equilibrium between  $\alpha$ - $\text{Al}_2\text{O}_3$ ,  $\beta$ - $\text{Al}_2\text{O}_3$  and liquid, it couldn't possibly terminate at the alumina corner. For many years  $\beta$ - $\text{Al}_2\text{O}_3$  was thought to be a metastable polymorph of corundum. In this event, an isotherm would likely separate the two fields rather than an univariant line. The work of DePable-Galan (5) in the  $\text{Na}_2\text{O-Al}_2\text{O}_3\text{-SiO}_2$  system refutes the notion of polymorphism and assigns a stable composition point to  $\beta$ - $\text{Al}_2\text{O}_3$  ( $\text{Na}_2\text{O} \cdot 11\text{Al}_2\text{O}_3$ ) on the  $\text{Na}_2\text{O-Al}_2\text{O}_3$  axis with eutectic points on both sides of the vertex. The  $\alpha$ - $\text{Al}_2\text{O}_3$ - $\beta$ - $\text{Al}_2\text{O}_3$  eutectic thus defined provides a terminus (that satisfies the phase rule) for the univariant line involving these phases rather than the alumina corner. However, if the view that the cryolite-alumina tie line separates the  $\alpha$ - and  $\beta$ - $\text{Al}_2\text{O}_3$  phase fields further in the diagram is valid, then the cryolite-alumina system doesn't possess a simple eutectic. A reaction point (peritectic) must exist at the minimum of the two intersecting liquidus curves where the three solid phases  $\alpha$ - $\text{Al}_2\text{O}_3$ ,  $\beta$ - $\text{Al}_2\text{O}_3$  and cryolite can exist in equilibrium with the liquid phase. Recent papers describing the phase relationships in the cryolite-alumina system (4, 7, 14) show conclusively that this is not the case. The publications of Albert and Breit (1), Pazukhin (12) and Arakelyan (2) report the identification of  $\beta$ - $\text{Al}_2\text{O}_3$  in basic cryolite-alumina melts. A peritectic reaction point is expected, if not on the cryolite-alumina join, then certainly on the sodium fluoride enriched side of that line. Phillips (13) gives liquidus isotherms on a  $\text{Na}_3\text{AlF}_6\text{-NaF-Al}_2\text{O}_3$  ternary plot, which indicate a peritectic close to the  $\text{Na}_3\text{AlF}_6\text{-Al}_2\text{O}_3$  binary ordinate. The experimental technique employed to determine these liquidus temperatures precludes identifying the equilibrium solid phases. The location of a ternary eutectic, however, is absent.

This paper gives the results of applying the quenching method to the determination of liquidus temperatures for

several sodium fluoride isocomposition sections and selected composition points in the  $\text{Na}_3\text{AlF}_6\text{-NaF-Al}_2\text{O}_3$  triangle. The weight % concentration terms employed in relation to the experimentally determined liquidus temperatures (Figures 1 and 2) and the subsequent location of phase fields in the composition triangle (Figure 3) are converted to reciprocal  $\text{Na}_6\text{F}_6\text{-Al}_2\text{F}_6\text{-Na}_6\text{O}_3\text{-Al}_2\text{O}_3$  quantities, facilitating the tracing of crystallization paths (Figure 4).

## EXPERIMENTAL

Details of the quenching procedure and the microscopy techniques used in the study of the quenched sample are essentially the same as described in a previous publication (6).

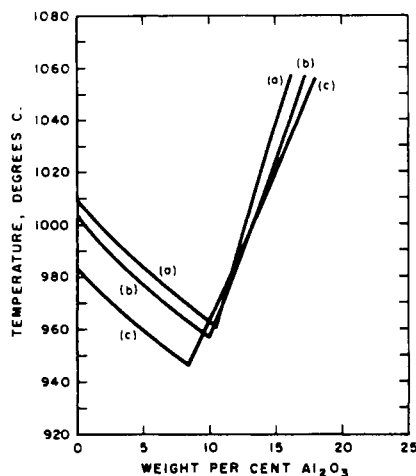


Figure 1. Liquidus curves; (a)  $\text{Na}_3\text{AlF}_6\text{-Al}_2\text{O}_3$  (b) 5 wt. % NaF section (c) 15 wt. % NaF section

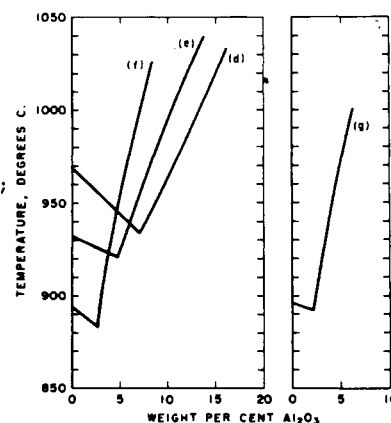


Figure 2. Liquidus curves; NaF sections, (d) 20 wt. % (e) 30 wt. % (f) 40 wt. % (g) 42 wt. %

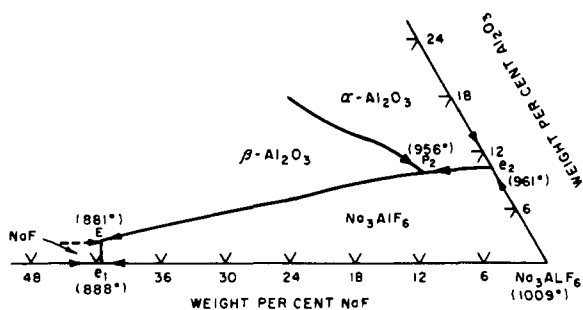


Figure 3. Location of phase fields in the cryolite corner of the  $\text{Na}_3\text{AlF}_6$ - $\text{NaF}$ - $\text{Al}_2\text{O}_3$  composition triangle

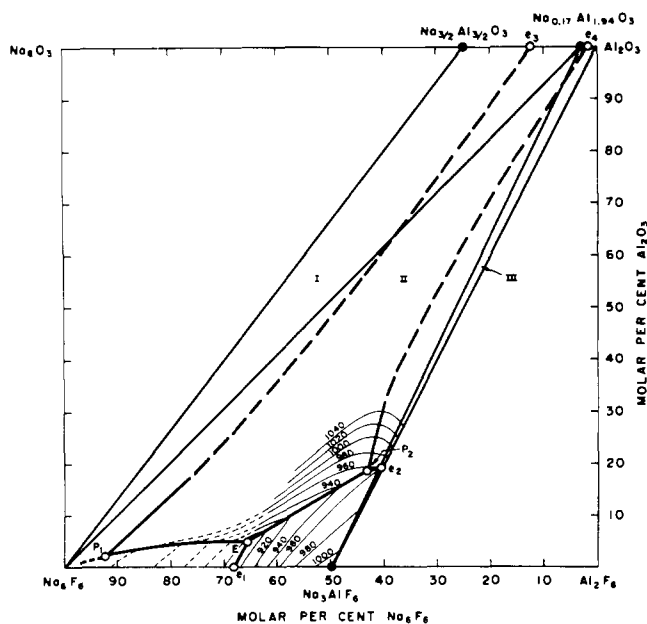


Figure 4. The reciprocal system  $\text{Na}_3\text{F}_6$ - $\text{Al}_2\text{F}_6$ - $\text{Na}_2\text{O}_3$ - $\text{Al}_2\text{O}_3$

Pt, Pt-10% Rh thermocouples were used to determine quenching temperatures. Calibration was based on an e.m.f. versus temperature curve employing the following fixed points: gold (wire), 1063°;  $\text{Na}_2\text{SO}_4$ , 884.8° and  $\text{NaCl}$ , 800.5° C.

Hand-picked, Greenland cryolite was used. The impurities were silicon ( $\text{SiO}_2$ ), 0.14%; potassium (KF), 0.005%; calcium ( $\text{CaF}_2$ ), 0.01%; and lithium (LiF), 0.035%. Sodium fluoride was certified by the Fisher Scientific Company as having the following impurities: iron, 0.002%; heavy metals as lead, 0.003%; water insoluble matter, 0.005%. The alumina used was Alcoa's A-14 grade. Predominant impurities in this material are soda, 0.092% and silica, 0.19%.

Ternary compositions low in sodium fluoride and alumina were pre-fused in a platinum crucible under argon, ground to pass 100-mesh size screen, homogenized by mechanical mixing and dried. Ten to fifteen milligrams was then charged into small platinum tubes and sealed. Other compositions, high in sodium fluoride and alumina, were weighed directly in the platinum tubes.

The identity of the precipitating primary phase particles ( $\text{Na}_3\text{AlF}_6$ ,  $\text{NaF}$ ,  $\beta\text{-Al}_2\text{O}_3$ ,  $\alpha\text{-Al}_2\text{O}_3$  and  $\text{NaAlO}_2$ ) was determined by refractive index measurements and x-ray powder diffraction.

## RESULTS AND DISCUSSION

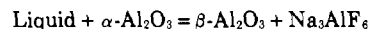
The shape of the primary phase surfaces, the location of univariant lines, and the invariant points in the cryolite

rich end of the  $\text{Na}_3\text{AlF}_6$ - $\text{NaF}$ - $\text{Al}_2\text{O}_3$  composition triangle were determined from the liquidus temperatures for the following NaF sections: 5, 15, 20, 30, 40 and 42 wt. %.

The liquidus curves for the 5 wt. % (b) and 15 wt. % (c) NaF sections and those of the cryolite-alumina system (a) are shown in Figure 1. The cryolite freezing point is depressed uniformly towards a minimum with increasing alumina content. The minimum represents a composition and temperature where the melts of a given section are doubly saturated with respect to cryolite and alumina. Each minimum defines a point of intersection with the ternary univariant line that originates at the cryolite-alumina eutectic.

As can be seen from Figure 1, the addition of NaF displaces the minimum toward lower alumina. At higher alumina contents than the double saturation point, the primary phase is alumina or an aluminate depending on the NaF content. System (a) and section (b) precipitate  $\alpha\text{-Al}_2\text{O}_3$ . Section (c), however, precipitates  $\beta\text{-Al}_2\text{O}_3$  as primary phase for compositions containing 8.4-17 wt. % alumina. Quenches of samples containing 18 wt. % alumina precipitate  $\alpha\text{-Al}_2\text{O}_3$ . The 15 wt. % NaF section cuts across  $\alpha$ -,  $\beta\text{-Al}_2\text{O}_3$  univariant line at high alumina contents (17-18 wt. %).

Several composition points were investigated to locate the  $\alpha$ -,  $\beta\text{-Al}_2\text{O}_3$  univariant line. Table I lists those that were helpful in defining that line and its inter-section with the cryolite-alumina univariant. A peritectic reaction point was located at 6.6 wt. % NaF, 9.9 wt. %  $\text{Al}_2\text{O}_3$  and 83.5 wt. %  $\text{Na}_3\text{AlF}_6$ , Figure 3, where  $\alpha\text{-Al}_2\text{O}_3$ ,  $\beta\text{-Al}_2\text{O}_3$  and  $\text{Na}_3\text{AlF}_6$  solid phases exist in equilibrium with liquid phase at 956°. Before the temperature can be reduced, the reaction



must progress to the complete consumption of  $\alpha\text{-Al}_2\text{O}_3$ .

Figure 1 shows that the slope of the alumina liquidus decreases with increasing NaF content. As a consequence, addition of NaF increases the solubility of  $\text{Al}_2\text{O}_3$  at high temperatures although the converse is true at low temperatures. For example at 970°, a melt containing cryolite and 15 wt. % NaF dissolves 10.6 wt. %  $\text{Al}_2\text{O}_3$ ; whereas cryolite alone dissolves 11.1 wt. %  $\text{Al}_2\text{O}_3$  at this temperature. However, at 1050° C. a cryolite-15 wt. % NaF melt can dissolve 17.5 wt. %  $\text{Al}_2\text{O}_3$  while cryolite alone dissolves only 15.7 wt. %  $\text{Al}_2\text{O}_3$ .

In sections (d), (e), and (f), Figure 2, cryolite precipitates as the primary phase on the low alumina side of the double saturation minimum. At higher alumina contents, the primary phase is  $\beta\text{-Al}_2\text{O}_3$ . The slopes of the alumina liquidus reverse the previous trend and increase with increasing sodium fluoride content.

In section (g), Figure 2, sodium fluoride rather than cryolite precipitates as the primary phase on the low alumina side of the double saturation minimum.  $\beta$ -alumina is the first crystal that forms from melts on the high alumina side.

With sections (f) [40 wt. % NaF] and (g) [42 wt. % NaF] cutting across the cryolite and sodium fluoride phase fields respectively, the following melt compositions were investi-

Table I. Composition Points and Related Primary Phases Used to Define the  $\alpha$ -,  $\beta\text{-Al}_2\text{O}_3$  Univariant Line

Composition (Wt. %)			Primary Phase
NaF	$\text{Al}_2\text{O}_3$	$\text{Na}_3\text{AlF}_6$	
7.0	11.0	82.0	$\alpha\text{-Al}_2\text{O}_3$
8.0	11.0	81.0	$\beta\text{-Al}_2\text{O}_3$
7.5	12.0	80.5	$\alpha\text{-Al}_2\text{O}_3$
8.8	12.0	79.2	$\beta\text{-Al}_2\text{O}_3$
13.5	16.0	70.5	$\alpha\text{-Al}_2\text{O}_3$
15.0	16.0	69.0	$\beta\text{-Al}_2\text{O}_3$

gated to locate the cryolite-sodium fluoride univariant line: 41 wt. % NaF, 1 wt. %  $\text{Al}_2\text{O}_3$ , 58 wt. %  $\text{Na}_3\text{AlF}_6$  and 41 wt. % NaF, 2 wt. %  $\text{Al}_2\text{O}_3$ , 57 wt. %  $\text{Na}_3\text{AlF}_6$ . The first of these compositions precipitated NaF and  $\text{Na}_3\text{AlF}_6$  simultaneously, and therefore, was judged to be located on the ternary univariant line. The second composition precipitates sodium fluoride as the primary phase. These two melt compositions and others located on sections (f) and (g) were triply saturated with respect to NaF,  $\text{Na}_3\text{AlF}_6$  and  $\beta\text{-Al}_2\text{O}_3$  at  $880^\circ\text{C}$ . The ternary eutectic was determined by a short extrapolation of univariant lines to occur at  $881^\circ\text{C}$  with a composition of 40.5 wt. % NaF, 2.3 wt. %  $\text{Al}_2\text{O}_3$ , and 57.2 wt. %  $\text{Na}_3\text{AlF}_6$ . The phase fields thereby defined are shown in Figure 3.

The ternary weight compositions of Figures 1, 2, 3 and Table I were converted to  $\text{Na}_6\text{F}_6$ ,  $\text{Al}_2\text{F}_6$ ,  $\text{Al}_2\text{O}_3$  reciprocal molar quantities. The appropriate liquidus temperatures were then utilized in plotting Figure 4.

The univariant line which separates the NaF and  $\beta\text{-Al}_2\text{O}_3$  phase fields was obtained by determining the primary phase for a number of compositions in that area. This line extends from E (Figure 4) towards the sodium fluoride-rich corner of the diagram, where it joins the NaF- $\text{NaAlO}_2$  and  $\beta\text{-Al}_2\text{O}_3$ - $\text{NaAlO}_2$  univariant lines at an invariant reaction point ( $P_1$ ). Liquidus temperatures, however, were not determined because of the steepness of the sodium aluminate and  $\beta$ -alumina surfaces. The composition of the peritectic,  $P_1$ , (92.1 mole %  $\text{Na}_6\text{F}_6$ , 5.5 mole %  $\text{Al}_2\text{F}_6$ , 2.4 mole %  $\text{Al}_2\text{O}_3$ ) differed slightly from the theoretical composition (92.7 mole %  $\text{Na}_6\text{F}_6$ , 3.4 mole %  $\text{Al}_2\text{F}_6$ , 3.8 mole %  $\text{Al}_2\text{O}_3$ ) which was based on secondary crystallization temperature of NaF- $\text{Al}_2\text{O}_3$  melts (8). The agreement, however, is good in view of the assumptions made in the theoretical calculations.

Table II summarizes data concerning composition, temperature, and the equilibrium solid phases for the various eutectic and peritectic points. The compositions of  $e_3$  and  $e_4$  were taken from the work of DePable-Galan (5).

The univariant line separating the sodium aluminate and  $\beta$ -alumina phase fields, starting at  $P_1$ , is extrapolated to join the eutectic of these same two compounds on the  $\text{Na}_6\text{O}_3$ - $\text{Al}_2\text{O}_3$  axis at  $e_3$ . Similarly, the univariant that defines the  $\alpha\text{-Al}_2\text{O}_3$  and  $\beta\text{-Al}_2\text{O}_3$  double saturation state starting at  $P_2$ , is extended to contact the binary eutectic at  $e_4$ . Interestingly, the region of maximum alumina solubility, as indicated by the humps in the isotherms, follows the penetration of the  $\alpha$ -,  $\beta\text{-Al}_2\text{O}_3$  univariant into the diagram.

#### CRYOLITE-SODIUM ALUMINATE SECTION

Interest in this system has been demonstrated by the appearance of several publications within the past decade dealing with liquidus temperatures (3), structural evaluations based on liquidus temperatures in cryolite-rich melts (10) and the identification of sub-liquidus sintered products (1).

The phase relationships for addition of sodium aluminate to cryolite can be derived from Figure 4 and compared to

earlier findings. Consider compositions along the line joining the cryolite ( $\text{Na}_6\text{F}_6/\text{Al}_2\text{F}_6 = 1$ ) and the sodium aluminate ( $\text{Na}_{3.2}\text{Al}_{3.2}\text{O}_3$ ) points for which liquidus temperatures are available. Figure 5 shows the vertical section for this system. The liquidus temperatures reported by Holm's (10) for compositions up to 6 mole % sodium aluminate are shown to agree with those taken from Figure 4. Bonnier (3) employed the thermal arrest method with fast cooling rates ( $10^\circ/\text{min.}$ ) and reports a eutectic at 49.8 mole %  $\text{NaAlO}_2$  and  $897^\circ\text{C}$ . The minimum in the liquidus curve of Figure 5 occurs at 23.5 mole % sodium aluminate and  $951^\circ$ . This minimum cannot be interpreted as a eutectic because the cryolite-sodium aluminate join is neither a "true" nor a "quasi" binary system. The reason being that the composition of the primary phase forming from the melt beyond the minimum is not located on the join. Compositions located between the cryolite vertex and the minimum precipitates cryolite as primary phase. The composition of the liquid phase follows the liquidus curve on further cooling until  $\beta\text{-Al}_2\text{O}_3$  forms from the melt at  $951^\circ\text{C}$ . A condition of univariant equilibrium is attained at this temperature. So that, on further cooling, the composition of the liquid phase departs from the cryolite-sodium aluminate join (Figure 5) and moves in the direction of E (Figure 4) along the line  $P_2 - E$  where the final products of crystallization are realized at  $881^\circ\text{C}$ . Somewhat differently, however, the composition of the liquid phase to the right of the liquidus minimum of Figure 5 departs immediately from the join on the appearance of primary phase  $\beta\text{-Al}_2\text{O}_3$ . The cryolite,  $\beta$ -alumina double saturation line is encountered at successively lower temperatures for starting compositions increasing in sodium aluminate content. These compositions, like all those located in conjugate sub-system II (Figure 4), ultimately became triply saturated with respect to sodium fluoride, cryolite and  $\beta$ -alumina at the invariant point E.

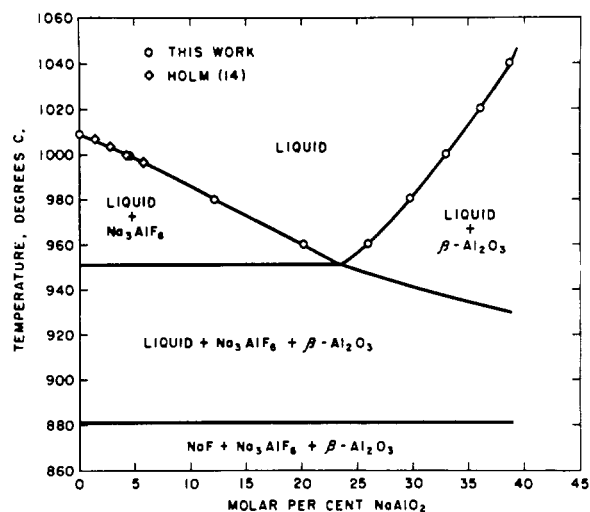


Figure 5. The  $\text{Na}_3\text{AlF}_6$ - $\text{NaAlO}_2$  section at the  $\text{Na}_6\text{F}_6$ - $\text{Al}_2\text{F}_6$ - $\text{Na}_6\text{O}_3$ - $\text{Al}_2\text{O}_3$  reciprocal section

Table II. Invariant Compositions, Temperatures and Related Equilibrium Solid Phases

Point	Composition				Temp., $^\circ\text{C}$ .	Solid Phases
	% $\text{Na}_6\text{F}_6$	% $\text{Al}_2\text{F}_6$	% $\text{Al}_2\text{O}_3$	% $\text{Na}_6\text{O}_3$		
$e_1$	68.4	31.6	...	...	888	$\text{Na}_3\text{AlF}_6$ , NaF
$e_2$	40.3	40.3	19.4	...	961	$\text{Na}_3\text{AlF}_6$ , $\text{Al}_2\text{O}_3$
$e_3$	...	...	87.5	12.5	...	$\text{NaAlO}_2$ , $\beta\text{-Al}_2\text{O}_3$
$e_4$	...	...	98.3	1.7	...	$\beta\text{-Al}_2\text{O}_3$ , $\alpha\text{-Al}_2\text{O}_3$
$P_1$	92.1	5.5	2.4	...	985	$\text{NaAlO}_2$ , $\beta\text{-Al}_2\text{O}_3$ , NaF
$P_2$	43.2	38.2	18.6	...	956	$\text{Na}_3\text{AlF}_6$ , $\beta\text{-Al}_2\text{O}_3$ , $\alpha\text{-Al}_2\text{O}_3$
E	65.2	29.8	5.0	...	881	$\text{Na}_3\text{AlF}_6$ , $\beta\text{-Al}_2\text{O}_3$ , NaF

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# Solid Compound Formation in the $\text{CCl}_4$ Mixtures of $p$ -Dioxane with $\text{CCl}_4$ , $\text{CBrCl}_3$ , and $\text{CFCl}_3$ . Solid-Liquid Phase Equilibria in Binary and $\text{CFCl}_3$ Systems

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Solid-liquid phase diagrams have been obtained from time-temperature cooling curves for the three binary systems formed from  $p$ -dioxane with  $\text{CCl}_4$ ,  $\text{CFCl}_3$ , and  $\text{CBrCl}_3$ . Solid compounds with the empirical formulas of  $p\text{-C}_4\text{H}_8\text{O}_2 \cdot (\text{CCl}_4)_2$  and  $p\text{-C}_4\text{H}_8\text{O}_2 \cdot (\text{CFCl}_3)_2$  were formed. The system  $p\text{-C}_4\text{H}_8\text{O}_2\text{-CBrCl}_3$  shows a maximum freezing point in a solid solution, but the evidence is against compound formation in that system. Exploratory measurements on the  $\text{CH}_3\text{CCl}_3$ -dioxane and  $(\text{CH}_3)_3\text{CCl}$ -dioxane systems show that they do not form compounds. These results are in qualitative agreement with the concept that  $p$ -dioxane is acting as an electron donor and the halogenated molecules as acceptors in the intermolecular compounds.

PREVIOUS PHASE DIAGRAM studies have shown that  $\text{CCl}_4$  forms solid compounds with benzene and several of its derivatives (2, 3, 6, 7, 9, 11, 12). Each of the aromatic substances that is known to form the  $\text{CCl}_4$  addition compound is characterized by a high electron density in the benzene ring, which suggests that the aromatic compound acts as a donor in a charge-transfer process. This explanation is supported by x-ray diffraction work on the related  $\text{CBr}_4$ - $p$ -Xylene system (13).

Other molecules capable of acting as electron donors might also form compounds with  $\text{CCl}_4$ . Dioxane appears to meet the requirements for a donor molecule; and it is known to form a compound with  $\text{CCl}_4$  (8).

This paper reports a solid-liquid phase equilibria study of  $p$ -dioxane with  $\text{CCl}_4$  (a more detailed study than the earlier work referred to above),  $\text{CBrCl}_3$ , and  $\text{CFCl}_3$ . The selection of the three halogen compounds, all of roughly the same shape and size, made possible a study of the effect of electronegativity of a substituent atom in  $\text{CCl}_4$  on the ability to form the intermolecular compound.

## EXPERIMENTAL

**Chemicals.** Starting materials were spectro-grade  $p$ -dioxane and reagent grade  $\text{CCl}_4$ ,  $\text{CBrCl}_3$ , and  $\text{CFCl}_3$ . The

dioxane,  $\text{CCl}_4$ , and  $\text{CFCl}_3$  were purified by fractional distillation in a vacuum-jacketed 100-cm. column packed with glass helices and operated at a reflux ratio of approximately 50:1. The  $\text{CBrCl}_3$ , because it showed signs of some decomposition (yellow color) under the conditions that the other substances were distilled, was vacuum distilled at room temperature in a 170-cm. long, glass helices packed distillation column and then fractionally crystallized once. The entire distillation apparatus was shielded from light by wrapping it in aluminum foil, since there was evidence for photochemical as well as thermal decomposition of this material.

With the exception of the  $\text{CBrCl}_3$ , which is discussed below, the purity of the products was determined from their time-temperature freezing curves. Calculations of the change in melting point as a function of the fraction melted showed the following liquid soluble-solid insoluble impurities present:  $p$ -dioxane, 0.06 mole %;  $\text{CCl}_4$ , 0.02 mole %; and  $\text{CFCl}_3$ , 0.05 mole %. The  $\text{CH}_3\text{CCl}_3$  and  $(\text{CH}_3)_3\text{CCl}$  used in the exploratory measurements were also purified by fractional distillation.

Because of the physical properties of the  $\text{CBrCl}_3$  (hard and massive crystals and small heat of fusion), it was difficult to obtain equilibrium conditions between solid and liquid, and the freezing curve for this substance was